# The Fabry-Perot Cavity

We will consider for simplicity a symmetric Fabry-Perot cavity. The boundaries of the Fabry-Perot are air (outside, medium 1) glass (inside, medium 2) interfaces. We will use the following notations:

- $\tilde{t}_{12}$  = transmission from outside (1) to inside (2)
- $\tilde{t}_{21}$  = transmission from inside (2) to outside (1)
- $\tilde{r}_{12}$  = reflection from outside (1) to inside (2)
- $\tilde{r}_{21}$  = reflection from inside (2) to outside (1).

The incident field is a plane wave of amplitude unity.

## Field transmission

$$\mathcal{T} = \tilde{t}_{12}\tilde{t}_{21}e^{-ikd} \\
+ \tilde{t}_{12}\tilde{t}_{21} \left(e^{-2ikd} \cdot \tilde{r}_{21}\tilde{r}_{21}\right)e^{-ikd} \\
+ \tilde{t}_{12}\tilde{t}_{21}e^{-ikd} \left(e^{-2ikd} \cdot \tilde{r}_{21}\tilde{r}_{21}\right)^2 + \dots \\
= \tilde{t}_{12}\tilde{t}_{21}e^{-ikd}\frac{1}{1 - \tilde{r}_{21}^2e^{-2ikd}}.$$
(1)

#### Interface properties

For an asymmetric interface:

$$\tilde{t}_{12}\tilde{t}_{21} - \tilde{r}_{12}\tilde{r}_{21} = 1$$
(2)

and

$$\boxed{\tilde{r}_{12} = -\tilde{r}_{21}^*} \tag{3}$$

Equation (2) implies that we can do the following substitution in Eq. (1:

$$\tilde{t}_{12}\tilde{t}_{21} = 1 + \tilde{r}_{12}\tilde{r}_{21} = 1 - |r_{12}|^2 = 1 - R.$$
 (4)

The result for the field transmission is:

$$\mathcal{T}(\Omega) = \frac{(1-R)e^{-ikd}}{1-Re^{i\delta}}$$
(5)

where

$$\delta(\Omega) = 2\varphi_r - 2k(\Omega)d\tag{6}$$

## **Field reflection**

$$\mathcal{R}(\Omega) = \frac{\sqrt{R} \left( e^{i\delta} - 1 \right)}{1 - R e^{i\delta}}.$$
(7)

One can easily verify that, if — and only if — kd is real:

$$|\mathcal{R}|^2 + |\mathcal{T}|^2 = 1 \tag{8}$$

Equations (5) and (7) are the transfer functions for the Fourier transform of the field. The dependence on the frequency argument  $\Omega$  occurs through  $k = n(\Omega)\Omega/c$ .

### Examples

Transmission for a train of pulses. Fabry-Perot as a frequency filter.

# Transfer functions

A transfer function is the mathematical representation of the relation between the input and output of a system.

 $\mathcal{R}(\Omega), \mathcal{T}(\Omega)$  are examples of transfer functions for the field  $\tilde{\mathcal{E}}(\Omega)$ .

# **Frequency Filter**

Referring to Eq. (5),  $\delta = -2k(\Omega) d$  for normal incidence. For clarity, we will neglect the phase shift on reflection.

One can use either angular or cyclic frequencies:

$$\delta = -\frac{2nd}{c}\Omega \tag{9}$$

$$\delta = -\frac{4\pi nd}{c}\nu \tag{10}$$

There are two important parts in the transmission: its periodicity, i.e. the transmission takes the same value for increments of  $\delta$  by  $2N\pi$ . This is called the *free spectral range*. In angular frequencies:

$$\Delta\Omega_{\rm fsr} = \frac{\pi c}{nd} \tag{11}$$

In cyclic frequencies:

$$\Delta \nu_{\rm fsr} = \frac{c}{2nd} \tag{12}$$

The next important dependence is close to the peak transmission, which corresponds to  $\delta = 0$  or  $2N\pi$ . The best approach is to make the approximation of small  $\delta$  in the trigonometric function.

**WARNING** One cannot make the approximation of  $\delta$  small in  $\tilde{\mathcal{T}}$  and thereafter calculate  $T = |\tilde{\mathcal{T}}|^2$ . One has to FIRST calculate T, and THEREAFTER make the approximation of small  $\delta$ . The intensity transmission factor T is:

$$T = \frac{1}{1 + \frac{2R}{(1-R)^2} \cos \delta}.$$
(13)

The approximation  $\cos \delta \approx 1 - \delta^2/2$  in Eq. (13) yields:

$$T \approx \frac{1}{1 + \frac{R}{(1-R)^2}\delta^2}.$$
(14)

Making the approximation of small  $\delta$  in Eq. 5 first gives you a different result. The FWHM of this Lorentzian is:

$$\Delta \delta_{\rm res} = \frac{2(1-R)}{\sqrt{R}}.$$
(15)

This relation leads directly to the definition of the finesse, which is the ratio of the free spectral range  $(2\pi)$  to the linewidth:

$$F = \frac{\pi\sqrt{R}}{1-R}.$$
(16)

For the use of the Fabry-Perot as a Filter, one can define the FWHM in angular frequency

or cyclic frequency: 
$$\Delta \Omega_{\rm res} = \frac{c(1-R)}{nd\sqrt{R}} \quad (17)$$
$$\Delta \nu_{\rm res} = \frac{c(1-R)}{2\pi nd\sqrt{R}} \quad (18)$$

#### Fabry-Perot Cascade

Let us assume that the thinnest practical Fabry-Perot to be of 100  $\mu$ m thickness. The corresponding free spectral range is  $\Delta \nu_{\rm fs1} = 1.5 \cdot 10^{12}$  Hz. The bandwidth that needs to be filtered is often much larger. Let us assume a "square" bandwidth that covers exactly  $(2N + 1)\Delta\nu_{\rm fs1}$  We dan arrange to have the transmission peak of index zero just outside the band, the transmission peak of index 1 just inside, the transmission peak of index N + 1 in the middle, index 2N + 1 just inside and index 2N + 1 just outside.

We want to built a filter that leaves only one peak transmitted in that range. Let us use a Fabry Perot of approximately twice the thickness, and the same finesse. "Approximately twice the thickness" implies a free spectral range of

$$\Delta \nu_{\rm fs2} = \Delta \nu_{\rm fs1} \left(\frac{1-\epsilon}{2}\right). \tag{19}$$

Since the finesse is the same:

$$\Delta \nu_{\rm res2} \approx \frac{1}{2} \Delta \nu_{\rm res1}.$$
 (20)

We look now for conditions that will tell us what the minimum  $\Delta \nu_{res1}$  should be in order to have only the central peak surviving in the superposition of the two Fabry-Perots. The first condition is that the second peak from the center of the thicker FP does not overlap with the first peak away from the center of the thinner one:

$$\begin{array}{rcl} \Delta\nu_{\rm fs1} - 2\Delta\nu_{\rm fs2} &\geq & \Delta\nu_{\rm res1} \\ \epsilon \times \Delta\nu_{\rm fs1} &\geq & \Delta\nu_{\rm res1} \end{array} \tag{21}$$

The second condition is that the outer transmission peaks do not overlap:

$$(2N+1)\Delta\nu_{\rm fs2} - N\Delta\nu_{\rm fs1} \geq \Delta\nu_{\rm res1}$$
$$\left[\frac{1}{2} - (N+\frac{1}{2})\epsilon\right]\Delta\nu_{\rm fs1} \geq \Delta\nu_{\rm res1}$$
(22)

which can be satisfied if  $\epsilon < 1/(2N+1)$ .

# Transmission/reflection for a monochromatic Gaussian beam

For a Gaussian beam:

$$\mathcal{E} = \mathcal{E}_0 e^{-r^2/w^2} \tag{23}$$

The Fourier transform along the transverse dimension is:

$$\mathcal{E}(\Delta k) = \int_{-\infty}^{\infty} \mathcal{E}(r) e^{i\Delta kr} dr \propto e^{-(\Delta k)^2 w^2/4}.$$
(24)

In the Fabry-Perot transmission function, we write  $\vec{k} = \vec{k_0} + \vec{\Delta k}$ , with the vector  $\vec{\Delta k}$  orthogonal to the vector  $\vec{k_0}$ . In the Fabry-Perot transmission function:

$$\delta = 2\varphi_r - 2\vec{k}_0 \cdot \vec{d} - 2\vec{\Delta k} \cdot \vec{d} = 2\varphi_r - 2k_0 d\cos\theta + 2\Delta k d\sin\theta = \delta_0 + 2a\Delta k, \quad (25)$$

with  $a = d \sin \theta$  To first order, we can neglect the variation of  $\theta$  as compared to  $\Delta k$ , putting all the variation in  $\Delta k$ .

The transmission of a Gaussian beam to a Fabry-Perot — in k - space is:

$$e^{-(\Delta k)^2 w^2/4} \times \frac{(1-R)e^{-i(\vec{k_0}.\vec{d}+2a\Delta k)}}{1-Re^{i(\delta_0+2a\Delta k)}}$$
 (26)

One can get a lot of information from this expression, without having to make the inverse Fourier transform to the position space. The phase factor  $\vec{k_0} \cdot \vec{d} + 2a\Delta k$  disappears when on takes the absolute value square. The important phase factor is in the denominator:  $\delta_0 + 2a\Delta k$ .  $\Delta k$  varies essentially in the range  $\pm 1/w$ .

#### Near normal incidence

Depending on the exact angle of incidence,  $\delta_0$  can be close to 0 or  $\pi$ . The term  $2a\Delta k = 2\Delta kd\sin\theta$  varies between  $\pm 2(d/w)\sin\theta$ . Starting with no fringe, there will be one fringe across the beam if  $2(d/w)\sin\theta \geq 2\pi$ , i.e. narrow beam (w small) and/or long FP (d large).