**Previously** 

*Fiber modes* 
$$V = k_0 a \sqrt{n_1^2 - n_2^2}$$
 Single mode if V<2.405

#### How to flip from single mode to multimode in a single mode fiber

Tapering: a changes from 4  $\mu$ m to 5  $\mu$ m,  $\Delta n$  from 0.0049 to 0.445  $\sqrt{n_1^2 - n_2^2}$  changes from 0.119 to 1.043. V from 1.9 to 10.6

#### **Polarization rotation -- linear**

in PM fibers. Temp sensor, power meter, stabilization

#### Today

#### **Polarization rotation -- nonlinear**

In nonlinear optics, 1 + 1 = 3! (????????)

Cross phase modulation

Mode-locked fiber lasers

#### Velocities in fibers

Phase velocity, group velocity, velocity in gain/absorber

#### **Polarization rotation -- nonlinear**

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Application: Colliding pulse mode-locking



#### Cross phase modulation

The nonlinear index (Kerr effect) comes from:  $P_{NL} = \epsilon \chi^{(3)} \mathbf{E} \mathbf{E} \mathbf{E}$ 

Same k, different frequencies, or same frequency, different k.  $E = \mathcal{E}_1 e^{i\omega_1 t} + \mathcal{E}_2 e^{i\omega_2 t}$   $P_{NL} \propto \left(\mathcal{E}_1 \mathcal{E}_1^* + \mathcal{E}_2 \mathcal{E}_2^*\right) \mathcal{E}_1 e^{i\omega_1 t} + \ldots + \left(\mathcal{E}_1 \mathcal{E}_2^* e^{i(\omega_1 - \omega_2)t}\right) \mathcal{E}_2 e^{i\omega_2 t}$   $P_{NL}(\omega_j) \propto \chi^{(3)} \left(|\mathcal{E}_1|^2 + 2|\mathcal{E}_2|^2\right) \mathcal{E}_1 e^{i\omega_1 t}$   $\Delta n_j = n_2 |E_j|^2 + 2|E_{3-j}|^2$   $1 \qquad 1 \qquad 2$   $2 \qquad 2 \qquad 1$ 

Co-propagating beams in fibers:

$$\Delta \phi_{NL} = k_0 \Delta n \ell$$

### Polarization rotation

The nonlinear index (Kerr effect) comes from:  $P_{NL} = \epsilon \chi^{(3)} \mathbf{E} \mathbf{E} \mathbf{E}$ 

Same *k*, frequency, orthogonal polarization.

$$E = \mathcal{E}_x e^{i\omega t} + \mathcal{E}_y e^{i\omega t}$$

$$P_{NL} \propto \epsilon_0 \chi \sum_{j} \left[ E_i E_j E_j^* + E_j E_i E_j^* + E_j E_j E_i^* \right]$$

$$P_x = \epsilon_0 \chi \sum_{j}^{i} \left[ E_x E_y E_y^* + E_y E_x E_y^* + E_y E_y E_y^* + E_x E_x E_x E_x^* + E_x E_x E_x E_x^* + E_x E_x E_x E_x^* \right]$$

$$P_x = \epsilon_0 \chi \sum_{j}^{i} \left[ 3|E_x|^2 + 2|E_y|^2 \right] E_x$$

$$P_x = 3\epsilon_0 \chi \sum_{j}^{i} \left[ |E_x|^2 + \frac{2}{3}|E_y|^2 \right] E_x$$

$$\Delta n_{\mathrm{nl},x} = n_2 \left[ |\tilde{\mathcal{E}}_{0x}|^2 + \frac{2}{3} |\tilde{\mathcal{E}}_{0y}|^2 \right]$$
  
$$\Delta n_{\mathrm{nl},y} = n_2 \left[ |\tilde{\mathcal{E}}_{0y}|^2 + \frac{2}{3} |\tilde{\mathcal{E}}_{0x}|^2 \right].$$

In an element of thickness  $d_m$ , this induced birefringence leads to a phase change between the x and y components of the field vector

$$\Delta\Phi(t) = \frac{2\pi}{\lambda_{\ell}} \left(\Delta n_{\mathrm{nl},x} - \Delta n_{\mathrm{nl},y}\right) = \frac{2\pi n_2 d_m}{3\lambda_{\ell}} \left[ |\tilde{\mathcal{E}}_{0x}(t)|^2 - |\tilde{\mathcal{E}}_{0y}(t)|^2 \right]$$

The phase shift is time dependent, and, in combination with another element, can represent an intensity-dependent loss element. Consider a sequence of such birefringent element and a linear polarizer. The incident pulse is

 $\begin{aligned} \mathcal{E}_{0x}(t) &= \mathcal{E}_0(t) \cos \alpha \\ \mathcal{E}_{0y}(t) &= \mathcal{E}_0(t) \sin \alpha \end{aligned}$ 

The pass direction of the polarizer is at  $\alpha + 90^{\circ}$  resulting in zero transmission through the sequence for low-intensity light ( $\Delta \Phi \approx 0$ ). Neglecting a common phase the field components at the output of the nonlinear element are

$$\begin{aligned} \mathcal{E}'_x(t) &= \left[ \mathcal{E}_0(t) \cos \alpha \right] \cos(\omega_\ell t) \\ \mathcal{E}'_y(t) &= \left[ \mathcal{E}_0(t) \sin \alpha \right] \cos \left[ \omega_\ell t + \Delta \Phi(t) \right]. \end{aligned}$$

Next the pulse passes through the linear polarizer. The total transmitted field is the sum of the components from  $\mathcal{E}'_x(t)$  and  $\mathcal{E}'_y(t)$  along the polarizer's path direction

$$\mathcal{E}_{out}(t) = \mathcal{E}_0(t) \cos \alpha \sin \alpha \left\{ -\cos(\omega_\ell t) + \cos\left[\omega_\ell t + \Delta \Phi(t)\right] \right\}$$

The total output intensity  $I_{out}(t) = \langle \mathcal{E}^2(t) \rangle$  is



Let us now assume a Gaussian input pulse  $I_{in} = I_0 \exp \left[-2(t/\tau_G)^2\right]$  and parameters of the nonlinear element so that for the pulse center the phase difference

$$\Delta \Phi(t=0) = \frac{2\pi n_2 d_m}{3\lambda_\ell} \mathcal{E}_0^2(t=0) \left(\sin^2 \alpha - \cos^2 \alpha\right) = \pi.$$

For this situation we obtain a transmitted pulse

$$I_{out}(t) = \frac{1}{2} I_{in}(t) \left\{ 1 - \cos \left[ \pi e^{-2(t/\tau_G)^2} \right] \right\}.$$

The transmission is maximum (= 1) where the nonlinear element acts like a half-wave plate that rotates the polarization by 90°, lining it up with the pass direction of the polarizer. For the parameters chosen here this happens at the pulse center (t = 0). The phase shift  $\Delta \Phi$  is smaller away from the pulse center producing elliptically polarized output and an overall transmission that approaches zero in the pulse wings. Thus this sequence of elements can give rise to an intensity dependent transmission similar to a fast absorber.





The question of how to start the mode locking process is solved in several ways. Experimentally, the Polarization Controllers (PC) have the greatest effect, given sufficient gain in the cavity. By manually adjusting the 6 paddles, we can sometimes get lucky and find CWML pulses on the oscilloscope. In practice, looking at the time trace does not get us close enough. It is easy to miss the ML'ing by moving the PC too fast, or not fast enough, etc.. We can monitor the optical spectrum and see the broadening of the bandwidth in the output. The other method of starting the CWML is to find the ``sweet spots'' on the box or the table and hitting those spots.



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## Slab waveguide solution



In metallic waveguides

Phase velocity: 
$$v_p = \frac{\Omega}{\beta} = \frac{\Omega}{k \sin \theta_m}$$
  
Group velocity:  $\frac{1}{v_g} = \frac{d\beta}{d\Omega}$   $v_g = \frac{c}{n} \sin \theta_m$ 

Velocities in fiber?



V = 2.405





### GROUP VELOCITY APPLIES ONLY TO LINEAR DIELECTRICS



VOLUME 23, NUMBER 1

#### NONLINEAR AMPLIFICATION OF LIGHT PULSES

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FIG. 5. Diagram of setup: 1 - laser mirror, 2 - polarizer, 3 - Kerr cell, 4 - laser ruby crystal, 5 - glass plate, 6 - coaxial photocell, 7 - amplifier ruby crystal, 8 - Sl-14 oscilloscope, 9 - neutral light filters. The input mirror of the laser is at the end of crystal 4.

# The velocity of a pulse in a saturable gain medium

$$\frac{v}{c} = 1 + \frac{c\tau_p}{2}(\alpha - \gamma)$$

- c Speed of light in the gain
- $\tau_p$  Pulse duration
- $\alpha$  Small signal gain coefficient (per unit length)
- $\gamma$  Loss coefficient (per unit length)

# The velocity of a pulse in a ring fiber laser

$$\frac{\mathbf{v}}{\mathbf{c}} = 1 + \frac{\mathbf{c}\tau_{\mathbf{p}}}{2} \left(\alpha_0 \frac{\mathcal{P}}{\mathcal{P}_0} - \gamma\right)$$

- c Speed of light in the gain
- $\boldsymbol{\tau}_{\mathbf{p}}$  Pulse duration
- $\alpha$  Small signal gain coefficient (per unit length)
- $\alpha_0$  Small signal gain at the laser threshold

- $\gamma$  Loss coefficient (per unit length)
- $\mathcal{P}$  Pump power
- $\mathcal{P}_0$  Pump power at the laser threshold

### **Example of pulse velocity** >> *c* **in a fiber laser**







 $\Delta \mathcal{P} = \mathcal{P}_{cw} - \mathcal{P}_{ccw}$ 



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### The velocity of a pulse in a ring fiber laser



Speed of light in the gain  $\boldsymbol{\tau}_{\mathbf{p}}$  Pulse duration Loss coefficient (per unit length) γ С Small signal gain coefficient (per unit length) Pump power  $\mathcal{P}$ a  $\alpha_0$  Small signal gain at the laser threshold  $\mathcal{P}_0$  Pump power at the laser threshold 400-Experiment ······ Kerr effect Basov theory 300 **ΔL (μm)** 200 100-0. 100 50 150 N

Pump power difference (mW)

**Parenthesis: the frequency comb** 



